

# Thermal Stresses of Semi Infinite Rectangular Beam with Internal Heat Source: Steady-State Problem

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*Abstract- This paper is concerned with inverse transient thermoelastic problem in which we need to determine the temperature distribution, displacement function and thermal stresses of a semi-infinite rectangular beam when the boundary conditions are known. Integral transform techniques are used to obtain the solution of the problem. The results are depicted graphically.*

**Key Words:** Semi-infinite rectangular beam, inverse transient problem, Integral transform.

## I. INTRODUCTION

**Khobragade et al.** [2-7, 9] have investigated temperature distribution, displacement function, and stresses of a thin rectangular plate and **Khobragade et al.** [8] have established displacement function, temperature distribution and stresses of a semi-infinite rectangular beam.

In this Section, an attempt has been made to determine the temperature distribution, unknown temperature gradient, displacement function and thermal stresses of a semi-infinite rectangular beam occupying the region  $D : -a \leq x \leq a ; 0 \leq y \leq b, 0 \leq z \leq \infty$  with known boundary conditions. Here Marchi-Fasulo transforms and Fourier cosine transform techniques have been used to find the solution.

## II. STATEMENT OF THE PROBLEM

Consider a thin rectangular plate occupying the space  $D : a \leq x \leq a ; 0 \leq y \leq b, 0 \leq z \leq \infty$ . The displacement components  $u_x$  and  $u_y$   $u_z$  in the x and y and z directions respectively as **Tanigawa et al.** [1] are

$$u_x = \int_{-a}^a \left[ \frac{1}{E} \left( \frac{\partial^2 U}{\partial y^2} + \frac{\partial^2 U}{\partial z^2} - \nu \frac{\partial^2 U}{\partial x^2} \right) + \lambda T \right] dx \quad (1)$$

$$u_y = \int_0^b \left[ \frac{1}{E} \left( \frac{\partial^2 U}{\partial z^2} + \frac{\partial^2 U}{\partial x^2} - \nu \frac{\partial^2 U}{\partial y^2} \right) + \lambda T \right] dy \quad (2)$$

$$u_z = \int_0^\infty \left[ \frac{1}{E} \left( \frac{\partial^2 U}{\partial x^2} + \frac{\partial^2 U}{\partial y^2} - \nu \frac{\partial^2 U}{\partial z^2} \right) + \lambda T \right] dz \quad (3)$$

where E,  $\nu$ , and  $\lambda$  are the young's modulus, Poisson's ratio and the linear coefficient of the thermal expansion of the material of the beam respectively and  $U(x,y,z)$  is the

Airy's stress functions which satisfy the differential equation as **Tanigawa et al.** [1] is

$$\left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \right)^2 U(x,y,z) = -\lambda E \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \right) T(x,y,z) \quad (4)$$

where  $T(x,y,z)$  denotes the temperature of a rectangular beam satisfy the following differential equation as **Tanigawa et al.** [1] is

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} + \frac{g(x,y,z)}{k} = 0 \quad (5)$$

where  $k$  is the thermal conductivity and  $\alpha$  is the thermal diffusivity of the material, subject to the boundary conditions

$$\left[ T(x,y,z) + k_1 \frac{\partial T(x,y,z)}{\partial x} \right]_{x=a} = f_1(y,z) \quad (6)$$

$$\left[ T(x,y,z) + k_2 \frac{\partial T(x,y,z)}{\partial x} \right]_{x=-a} = f_2(y,z) \quad (7)$$

$$\left[ \frac{\partial T(x,y,z)}{\partial y} \right]_{y=0} = f_3(x,z) \quad (8)$$

$$\left[ \frac{\partial T(x,y,z)}{\partial y} \right]_{y=b} = f_4(x,z) \quad (9)$$

$$[T(x,y,z)]_{y=b} = G(x,z) \text{ (Unknown)} \quad (10)$$

$$[T(x,y,z)]_{z=0} = 0 \quad (11)$$

$$[T(x,y,z)]_{z=\infty} = 0 \quad (12)$$

The stress components in terms of  $U(x,y,z)$  **Tanigawa et al.** [1] are given by

$$\sigma_{xx} = \left[ \frac{\partial^2 U}{\partial y^2} + \frac{\partial^2 U}{\partial z^2} \right] \quad (13)$$

$$\sigma_{yy} = \left[ \frac{\partial^2 U}{\partial z^2} + \frac{\partial^2 U}{\partial x^2} \right] \tag{14}$$

$$\sigma_{zz} = \left[ \frac{\partial^2 U}{\partial x^2} + \frac{\partial^2 U}{\partial y^2} \right] \tag{15}$$

The equations (1) to (15) constitute the mathematical formulation of the problem under consideration.

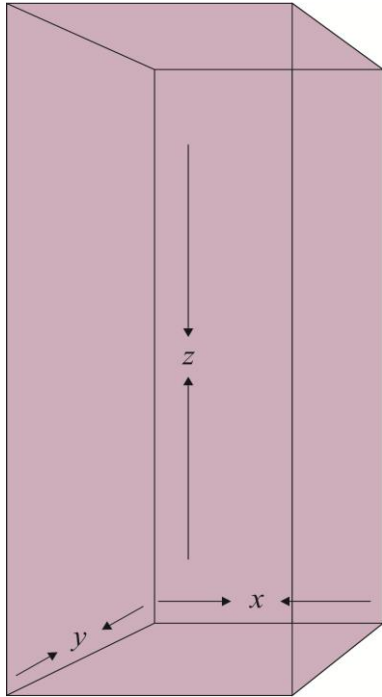


Fig 1: Geometry of the problem

### III. SOLUTION OF THE PROBLEM

Applying finite Marchi-Fasulo transform and Fourier sine transform to the equation (5), we get

$$\frac{d\bar{T}^*}{dt} - q^2 \bar{T}^* = \Psi \tag{16}$$

Where,  $q^2 = \lambda_n^2 + p^2$

$$\Psi = \frac{P_n(-a)}{k_2} f_2^* - \frac{P_n(a)}{k_1} f_1^* - \frac{\bar{g}^*}{k}$$

Equation (16) is a linear equation whose solution is given by

$$\bar{T}^* = Ae^{qy} + Be^{-qy} + F(y) \tag{17}$$

Where  $F(y)$  is the P.I.

Using boundary conditions (8) and (9) we get

$$A = \frac{e^{-q\xi} (F'(0) - \bar{f}_3^*) + F'(\xi)}{2q \sinh(q\xi)}$$

$$B = \frac{e^{q\xi} (F'(0) - \bar{f}_3^*) + \bar{f}_4^* - F'(\xi)}{2q \sinh(q\xi)}$$

Substituting the values of A and B in equation (17) one obtains

$$\bar{T}^* = \frac{[(F'(0) - \bar{f}_3^*) \cosh(q(y - \xi)) + (\bar{f}_4^* - F'(\xi)) \cosh(qy)]}{q \sinh(q\xi)} + F(y) \tag{18}$$

Applying inverse Fourier sine transform and inverse Marchi-Fasulo transform on equation (18) we get,

$$T = \frac{2}{\pi} \sum_{n=1}^{\infty} \frac{P_n(x)}{\lambda_n} \times \int_0^{\infty} \left\{ \frac{(F'(0) - \bar{f}_3^*) \cosh \sqrt{p^2 + \lambda_n^2} (y - \xi) + (\bar{f}_4^* - F'(\xi)) \cosh(\sqrt{p^2 + \lambda_n^2} y)}{\sqrt{p^2 + \lambda_n^2} \sinh(\xi \sqrt{p^2 + \lambda_n^2})} + F(y) \right\} \times \sin(pz) dp \tag{19}$$

$$G = \frac{2}{\pi} \sum_{n=1}^{\infty} \frac{P_n(x)}{\lambda_n} \times \int_0^{\infty} \left\{ \frac{(F'(0) - \bar{f}_3^*) \cosh \sqrt{p^2 + \lambda_n^2} (b - \xi) + (\bar{f}_4^* - F'(\xi)) \cosh(\sqrt{p^2 + \lambda_n^2} b)}{\sqrt{p^2 + \lambda_n^2} \sinh(\xi \sqrt{p^2 + \lambda_n^2})} + F(b) \right\} \times \sin(pz) dp \tag{20}$$

### IV. AIRY'S STRESS FUNCTIONS

Substituting the value of temperature distribution  $T(x,y,z)$  from (19) in equation (4) one obtains

$$U = \frac{-2\lambda E}{\pi} \sum_{n=1}^{\infty} \frac{P_n(x)}{\lambda_n} \times \int_0^{\infty} \left\{ \frac{(F'(0) - \bar{f}_3^*) \cosh \sqrt{p^2 + \lambda_n^2} (y - \xi) + (\bar{f}_4^* - F'(\xi)) \cosh(\sqrt{p^2 + \lambda_n^2} y)}{\sqrt{p^2 + \lambda_n^2} \sinh(\xi \sqrt{p^2 + \lambda_n^2})} + F(y) \right\} \times \sin(pz) dp \tag{20}$$

### V. DISPLACEMENT COMPONENTS

Substituting the values of Airy's stress function from equation (20) in the equation (1) to (3), one obtains

$$u_x = \frac{-2\lambda}{\pi} \int_{-a}^a \int_0^\infty \sum_{n=1}^\infty \frac{1}{\lambda_n} \left\{ \frac{(F'(0) - \bar{f}_3^*) \cosh \sqrt{p^2 + \lambda_n^2} (y - \xi) + (\bar{f}_4^* - F'(\xi)) \cosh(\sqrt{p^2 + \lambda_n^2} y)}{\sqrt{p^2 \lambda_n^2} \sinh(\xi \sqrt{p^2 + \lambda_n^2})} \right. \\ \left. + [F''(y) - (p^2 + 1)F(y)] P_n(n) - \nu F(y) P_n''(n) \right\} \sin(pz) dp dx \quad (21)$$

$$u_y = \frac{2\lambda}{\pi} \int_{-a}^b \int_0^\infty \sum_{n=1}^\infty \frac{1}{\lambda_n} \left\{ \frac{(F'(0) - \bar{f}_3^*) \cosh(\sqrt{p^2 + \lambda_n^2} (y - \xi)) + (\bar{f}_4^* - F'(\xi)) \cosh(\sqrt{p^2 + \lambda_n^2} y)}{\sqrt{p^2 \lambda_n^2} \sinh(\xi \sqrt{p^2 + \lambda_n^2})} \right. \\ \left. + [(v+1)P^2 + \nu \lambda_n^2 + 1] P_n(x) - \nu P_n''(x) \right\} \\ + [(P^2 + 1)F(y) + \nu F''(y)] P_n(n) - F(y) P_n''(n) \sin(pz) dp dy \quad (22)$$

$$u_z = \frac{-2\lambda}{\pi} \int_0^\infty \int_0^\infty \sum_{n=1}^\infty \frac{1}{\lambda_n} \left\{ \frac{(F'(0) - \bar{f}_3^*) \cosh \sqrt{p^2 + \lambda_n^2} (y - \xi) + (\bar{f}_4^* - F'(\xi)) \cosh(\sqrt{p^2 + \lambda_n^2} y)}{\sqrt{p^2 \lambda_n^2} \sinh(\xi \sqrt{p^2 + \lambda_n^2})} \right. \\ \left. + [(v-1)P^2 + \lambda_n^2 - 1] P_n(x) + P_n''(x) \right\} \\ + [(v P^2 - 1)F(y) + \nu F''(y)] P_n(n) + F(y) P_n''(n) \times \sin(pz) dp dz \quad (23)$$

**VI. DETERMINATION OF STRESS FUNCTION**

Substituting the value of Airy's stress function U(x,y,z) from equation (20) in the equation (14) to (16) one obtain the stress functions as,

$$\sigma_{xn} = \frac{-2\lambda E}{\pi} \sum_{n=1}^\infty \int_0^\infty \frac{P_n(x)}{\lambda_n}$$

$$\left\{ \frac{(F'(0) - \bar{f}_3^*) \cosh \sqrt{p^2 + \lambda_n^2} (y - \xi) + (\bar{f}_4^* - F'(\xi)) \cosh(\sqrt{p^2 + \lambda_n^2} y)}{\sqrt{p^2 \lambda_n^2} \sinh(\xi \sqrt{p^2 + \lambda_n^2})} \right. \\ \left. + F''(y) - P^2 F(y) \right\} \sin(pz) dp \quad (24)$$

$$\sigma_{yy} = \frac{2\lambda E}{\pi} \sum_{n=1}^\infty \int_0^\infty \frac{P_n(x) - P_n''(x)}{\lambda_n} \left[ \frac{(F'(0) - \bar{f}_3^*) \cosh \sqrt{p^2 + \lambda_n^2} (y - \xi) + (\bar{f}_4^* - F'(\xi)) \cosh(\sqrt{p^2 + \lambda_n^2} y)}{\sqrt{p^2 \lambda_n^2} \sinh(\xi \sqrt{p^2 + \lambda_n^2})} + F(y) \right] \sin(pz) dp \quad (25)$$

$$\sigma_{zz} = \frac{-2\lambda E}{\pi} \sum_{n=1}^\infty \int_0^\infty \frac{1}{\lambda_n} \left\{ \frac{(F'(0) - \bar{f}_3^*) \cosh \sqrt{p^2 + \lambda_n^2} (y - \xi) + (\bar{f}_4^* - F'(\xi)) \cosh(\sqrt{p^2 + \lambda_n^2} y)}{\sqrt{p^2 \lambda_n^2} \sinh(\xi \sqrt{p^2 + \lambda_n^2})} \right. \\ \left. + [(P^2 + \lambda_n^2) P_n(x) + P_n''(x)] + F''(y) P_n(x) + F(y) P_n''(x) \right\} \sin(pz) dp \quad (26)$$

Equations (20) and (21) are the required solutions.

**VII. SPECIAL CASE**

Set

$$f(x, y, z, t) = (x - a)^2 (x + a)^2 (z + e^{-z})(e^{y-t})$$

$$\bar{f}(n, y, z, t) = (z + e^{-z})(e^{y-t})$$

$$\times \left[ \frac{a_n \cos^2(a_n a) - \cos(a_n a) \sin(a_n a)}{a_n^2} \right]$$

Substituting this value in equation (20) we get

$$G = \frac{2}{\pi} \sum_{n=1}^\infty \frac{P_n(x)}{\lambda_n}$$

$$\int_0^{\infty} \left\{ \frac{(F'(0) - \bar{f}_3^*) \cosh \sqrt{p^2 + \lambda_n^2} (b - \xi)}{(\bar{f}_4^* - F'(\xi)) \cosh \left( \sqrt{p^2 + \lambda_n^2} b \right)} + F(b) \right\} \frac{1}{\sqrt{p^2 \lambda_n^2 \sinh \left( \xi \sqrt{p^2 + \lambda_n^2} \right)}} \sin(pz) dp \quad (27)$$

### VIII. NUMERICAL RESULTS

Set  $a = 2$ ,  $k = 0.86$ ,  $b = 3$ ,  $\xi = 2$ ,  $t = 1$  sec in the equations (20) to obtain

$$G = \frac{2}{\pi} \sum_{n=1}^{\infty} \frac{P_n(x)}{\lambda_n} \int_0^{\infty} \left\{ \frac{(F'(0) - \bar{f}_3^*) \cosh \sqrt{p^2 + \lambda_n^2} y}{(\bar{f}_4^* - F'(2)) \cosh \left( \sqrt{p^2 + \lambda_n^2} y \right)} + F(3) \right\} \frac{1}{\sqrt{p^2 \lambda_n^2 \sinh \left( \xi \sqrt{p^2 + \lambda_n^2} \right)}} \sin(pz) dp \quad (28)$$

### IX. MATERIAL PROPERTIES

The numerical calculations has been carried out for an Aluminum (pure) rectangular beam with the material properties as,

Density  $\rho = 169$  lb/ft<sup>3</sup>

Specific heat = 0.208 Btu/lbOF

Thermal conductivity  $K = 117$  Btu/(hr. ftOF)

Thermal diffusivity  $\alpha = 3.33$  ft<sup>2</sup>/hr.

Poisson ratio  $\nu = 0.35$

Coefficient of linear thermal expansion  $\alpha_t = 12.84 \times 10^{-6}$  1/F

Lame constant  $\mu = 26.67$

Young's modulus of elasticity  $E = 70G$  Pa

### X. DIMENSIONS

The constants associated with the numerical calculation are taken as

Length of rectangular beam  $x = 4$ ft

Breath of rectangular beam  $y = 3$  ft

Height of rectangular beam  $z = 10^3$ ft

### XI. CONCLUSION

In this article, the temperature distribution, unknown temperature gradient, displacement function and thermal stresses of a semi-infinite rectangular beam have been obtained, when the boundary conditions are known with the aid of finite Marchi-Fasulo transform and semi-infinite Fourier cosine transform techniques. The results are obtain

in the form of infinite series in terms of Bessel's function and depicted graphically.

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### AUTHOR BIOGRAPHY



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